

# **XR620A** Instrumentation Amplifier

# **General Description**

The XR620A is a low power, general purpose instrumentation amplifier with a gain range of 1 to 10,000. The XR620A is offered in 8-lead SOIC or DIP packages and requires only one external gain setting resistor making it smaller and easier to implement than discrete, 3-amp designs.

While consuming only 2.2mA of supply current, the XR620A offers a low 6.6nV/Hz input voltage noise and 0.2µVpp noise from 0.1Hz to 10Hz.

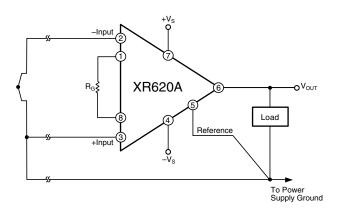
The XR620A offers a low input offset voltage of ±125µV that only varies 0.1µV/°C over it's operating temperature range of -40°C to +85°C. The XR620A also features 50ppm maximum nonlinearity. These features make it well suited for use in data acquisition systems.

#### **FEATURES**

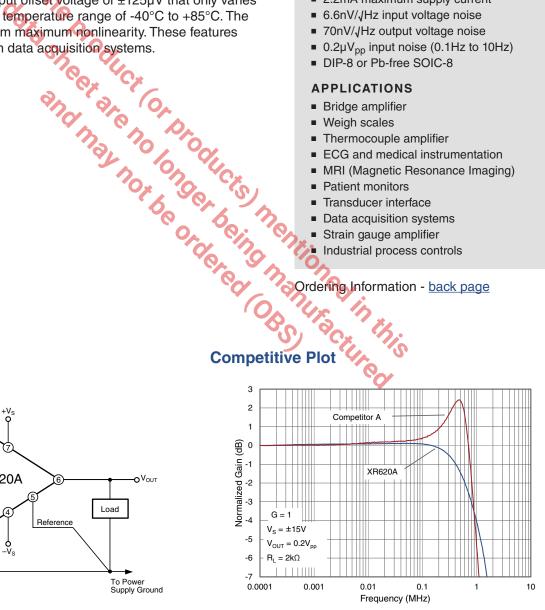
- ±2.3V to ±18V supply voltage range
- Gain range of 1 to 10,000
- Gain set with one external resistor
- ±125µV maximum input offset voltage
- 0.1µV/°C input offset drift
- 700kHz bandwidth at G = 1
- 1.2V/µs slew rate
- 90dB minimum CMRR at G = 10
- 2.2mA maximum supply current
- 6.6nV/√Hz input voltage noise
- 0.2µV<sub>pp</sub> input noise (0.1Hz to 10Hz)

- ECG and medical instrumentation
- MRI (Magnetic Resonance Imaging)

# **Typical Application**



Thermocouple Amplifier



# **Absolute Maximum Ratings**

Stresses beyond the limits listed below may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

Supply Voltage±18V
Input Voltage Range $\pm V_S  V$
Differential Input Voltage (G = 1 to 10) 25V
Differential Input Voltage (G > 10) $\leq$ 0.05 (R <sub>G</sub> + 800) +1 V
Load Resistance (min) $1\Omega$

# **Operating Conditions**

Supply Voltage Range	±2.3V to ±18V (4.6V to 36V)
Gain Range	1 to 10,000
Operating Temperature Range	-40°C to 85°C
Junction Temperature	
Storage Temperature Range	65°C to 150°C
Lead Temperature (Soldering, 10s) .	

# **Package Thermal Resistance**

e (G = 1 to 10)		Package Thermal Resistance	
$e (G > 10) \dots \le 0.05 (R_G + 800)$	+1 V	θ <sub>JA</sub> (DIP-8)	100°C/W
	1Ω	θ <sub>JA</sub> (SOIC-8)	150°C/W
d'a the		θ <sub>JA</sub> (DIP-8)         θ <sub>JA</sub> (SOIC-8)         Package thermal resistance (θ <sub>JA</sub> ), JEDEC statest boards, still air.         ESD Protection         SOIC-8 (HBM)         ESD Rating for HBM (Human Body Model).	ndard, multi-layer
Ta Dr		ESD Protection	
She di		SOIC-8 (HBM)	1.5kV
· · · · · · · · · · · · · · · · · · ·		ESD Rating for HBM (Human Body Model).	
an ar o			
mino	Dro		
al the	0,		
Or C	S.		
	00	6 nop	
	Ĩ,		
		ed lap ed	
		OB UT IN	
		S Ct. nis	
		e contraction de la contractica de la contractic	
		×	

SOIC-8 (HBM) 1.54	٢V
ESD Rating for HBM (Human Body Model).	

# **Electrical Characteristics**

 $T_A = 25^{\circ}C$ ,  $V_S = \pm 15V$ ,  $R_L = 2k\Omega$  to GND; unless otherwise noted. Gain = 1 + (49.4k/R\_G); Total RTI Error =  $V_{OSI}$  + ( $V_{OSO}/G$ )

Symbol	Parameter	Conditions	Min	Тур	Max	Units
Gain						
	Gain Range		1		10,000	
		$G = 1, V_{OUT} = \pm 10V$	-0.1		0.1	%
		$G = 10, V_{OUT} = \pm 10V$	-0.375		0.375	%
	Gain Error <sup>(1)</sup>	$G = 100, V_{OUT} = \pm 10V$	-0.375		0.375	%
		G = 1,000, V <sub>OUT</sub> = ±10V	-0.8		0.8	%
		G = 1 - 100, $V_{OUT}$ = -10V to 10V, $R_L$ = 10k $\Omega$		10	50	ppm
	Gain Nonlinearity	$G$ = 1 - 100, $V_{OUT}$ = -10V to 10V, $R_L$ = 2k $\Omega$		10	95	ppm
		G = 1		<10		ppm/°
	Gain vs. Temperature	G > 1		<-50		ppm/°(
	Reference Gain Error	$V_{S} = \pm 16.5 V$	-0.03		0.03	%
Voltage Offs	set					
V <sub>OSI</sub>	Input Offset Voltage	$V_{\rm S} = \pm 4.5 V$ to $\pm 16.5 V$	-125		125	μV
	Average Temperature Coefficient	$V_{\rm S} = \pm 4.5 V$ to $\pm 16.5 V$		0.1		µV/°C
V <sub>OSO</sub>	Output Offset Voltage	$V_8 = \pm 4.5V$ to $\pm 16.5V$ , G = 1	-1500	200	1500	μV
	Average Temperature Coefficient	$V_{S} = \pm 4.5V$ to $\pm 16.5V$		2.5		µV/°C
	<b>'</b>	$G = 1, V_S = \pm 2.3V$ to $\pm 18V$	80	100		dB
PSR	Offeet Deferred to the Input ve Supply	$G = 10, V_S = \pm 2.3V$ to $\pm 18V$	95	120		dB
ron	Offset Referred to the Input vs. Supply	$G = 100, V_S = \pm 2.3V$ to $\pm 18V$	110	140		dB
		$G = 1000, V_S = \pm 2.3V$ to $\pm 18V$	110	140		dB
Input Curre	nt					
I <sub>B</sub>	Input Bias Current	$V_{\rm S} = \pm 16.5 V$	-2	0.5	2	nA
	Average Temperature Coefficient	V <sub>S</sub> = ±16.5V		3		pA/°C
I <sub>OS</sub>	Input Offset Current	V <sub>S</sub> = ±16.5V	-1		1	nA
Input						
Input Impedance	Differential		10, 2		GΩ, pl	
	Common-Mode		10, 2		GΩ, pl	
IVR	Input Voltage Bange (2)	V <sub>S</sub> = ±4.5V, G = 1	-V <sub>S</sub> + 1.9		+V <sub>S</sub> - 1.2	V
IVR	Input Voltage Range (2)	V <sub>S</sub> = ±16.5V, G = 1	-V <sub>S</sub> + 1.9		+V <sub>S</sub> - 1.4	V
		G = 1, V <sub>S</sub> = ±16.5V	70 🗸	90		dB
CMRR	Common-Mode Rejection Ratio	$G = 10, V_S = \pm 16.5V$	90	110		dB
Civinn		$G = 100, V_S = \pm 16.5V$	108	130		dB
		$G = 1000, V_S = \pm 16.5V$	108	130		dB
Output						
V	Output Swing	$V_{\rm S} = \pm 2.3 V$ to $\pm 4.5 V$	-V <sub>S</sub> + 1.1		+V <sub>S</sub> - 1.2	V
V <sub>OUT</sub>	Output Swing	V <sub>S</sub> = ±18V, G = 1	-V <sub>S</sub> + 1.4		+V <sub>S</sub> - 1.2	V
I <sub>SC</sub>	Short Circuit Current			±20		mA
Dynamic Pe	erformance					
		G = 1		700		kHz
	Small Signal 2dD Danshuidth	G = 10		400		kHz
	Small Signal -3dB Bandwidth	G = 100		100		kHz
		G = 1000		12		kHz
SR	Slew Rate	$G = 10, V_S = \pm 15V$	0.6	1.2		V/µs
		5V step, G = 1 to 100		13		μs
t <sub>S</sub>	Settling Time to 0.01%	5V step, G = 1000		110		μs

# **Electrical Characteristics continued**

 $T_A = 25^{\circ}C$ ,  $V_S = \pm 15V$ ,  $R_L = 2k\Omega$  to GND; unless otherwise noted. Gain = 1 + (49.4k/R\_G); Total RTI Error =  $V_{OSI}$  + ( $V_{OSO}/G$ )

Symbol	Parameter	Conditions	Min	Тур	Max	Units
Noise						
e <sub>ni</sub>	Input Voltage Noise	1kHz, G = 1000, V <sub>S</sub> = ±15V		6.6	13	nV/√Hz
e <sub>no</sub>	Output Voltage Noise	1kHz, G = 1, V <sub>S</sub> = ±15V		70	100	nV/√Hz
		G = 1, 0.1Hz to 10Hz		5		μV <sub>pp</sub>
e <sub>npp</sub>	Peak-to-Peak Noise (RTI)	G = 10, 0.1Hz to 10Hz, V <sub>S</sub> = ±15V			0.8	μV <sub>pp</sub>
		G = 100, 0.1Hz to 10Hz, V <sub>S</sub> = ±15V		0.2	0.4	μV <sub>pp</sub>
i <sub>n</sub>	Current Noise	f = 1kHz		100		fA/√Hz
i <sub>npp</sub>	Peak-to-Peak Current Noise	0.1Hz to 10Hz		10		pA <sub>pp</sub>
Reference	Input					
R <sub>IN</sub>	Input Resistance			20		kΩ
I <sub>IN</sub>	Input Current	$V_{\rm S} = \pm 16.5 V$		50	60	μA
	Voltage Range		-V <sub>S</sub> + 1.6		+V <sub>S</sub> - 1.6	V
	Gain to Output	O.		1±0.0001		
Power Sup	ply	40.				
Vs	Operating Range		±2.3		±18	V
I <sub>S</sub>	Supply Current	$V_{\rm S} = \pm 16.5 V$		1.3	2.2	mA

#### Notes:

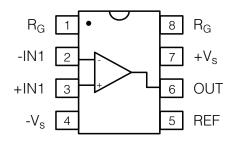
1. Nominal reference voltage gain is 1.0

2. Input voltage range = CMV + (G  $V_{DIFF}$ )/2

Vs = ±10.5V Vs =

# XR620A Pin Configurations

# SOIC-8, DIP-8



# **XR620A Pin Assignments**

## SOIC-8, DIP-8

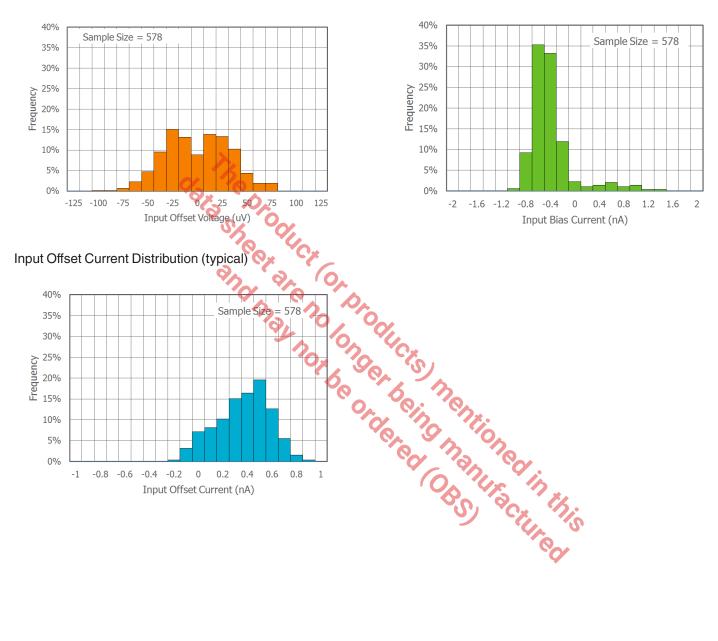
Pin No.	Pin Name	Description
1, 8	R <sub>G</sub>	R <sub>G</sub> sets gain
2	-IN	Negative input
3	+IN	Positive input
4	-V <sub>S</sub>	Negative supply
5	REF	Output is referred to the REF pin potential
6	OUT	Output
7	+V <sub>S</sub>	Positive supply

The product or products mentioned in this ordered or deside the interview of the interview

 $T_A = 25^{\circ}C$ ,  $V_S = \pm 15V$ ,  $R_L = 2k\Omega$  to GND; unless otherwise noted.

#### Input Offset Distribution (typical)

Input Bias Current Distribution (typical)



 $T_A$  = 25°C,  $V_S$  = ±15V,  $R_L$  = 2k $\Omega$  to GND; unless otherwise noted.

#### Gain vs. Frequency

70 +V<sub>s</sub> - 1.5 Ġ = 10  $R_1 = 2k\Omega$ 60 G = 1000 1  $R_L = 10 k\Omega$ 50 Output Voltage Swing (V) <sup>50</sup> <sup>60</sup> <sup>60</sup> <sup>60</sup> <sup>60</sup> 40 G = 100 Gain (dB) 30 20 G = 10 10  $R_L = 10 k\Omega$ 0  $R_L = 2k\Omega$ -10 ferred to Supply Voltages -20 0.0001 0.001 0.01 0.1 5 10 15 20 0.01 Frequency (MHz) Supply Voltage (+/- V) heer a Input Voltage Range vs. VS Output Voltage Swing vs. R +V<sub>s</sub>- 2 G = 10 Referred to Supply Input Voltage Swing (V) 0 -V<sub>s</sub>+ 2 0.1 10 1 0 5 10 15 Load Resistance (kΩ) Supply Voltage (+/- V) Large Signal Settling Time (G = 1)Large Signal Pulse Response (G = 1) 7.5  $G = 1, R_L = 2K$ 0.09 G = 1, 5V Step 5 0.08 0.07 Output Voltage (V) 0 -2.5 Output Settling (%) 0.06 0.05 0.04 0.03 0.02 0.01 -5 0 -7.5 -0.01 0 20 80 5 40 60 100 0 10 15 20 25 30 35 40 45

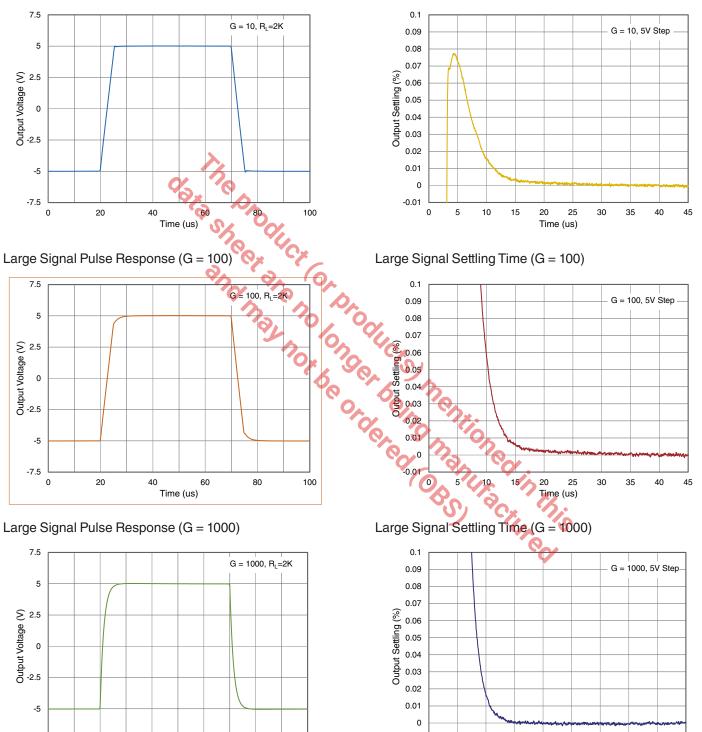
Output Voltage Swing vs. VS

Time (us)

Time (us)

 $T_A = 25^{\circ}C$ ,  $V_S = \pm 15V$ ,  $R_L = 2k\Omega$  to GND; unless otherwise noted.

Large Signal Pulse Response (G = 10)



Large Signal Settling Time (G = 10)

200

400

Time (us)

600

800

1000

-7.5

0

-0.01

0

50

100

150

200

Time (us)

250

300

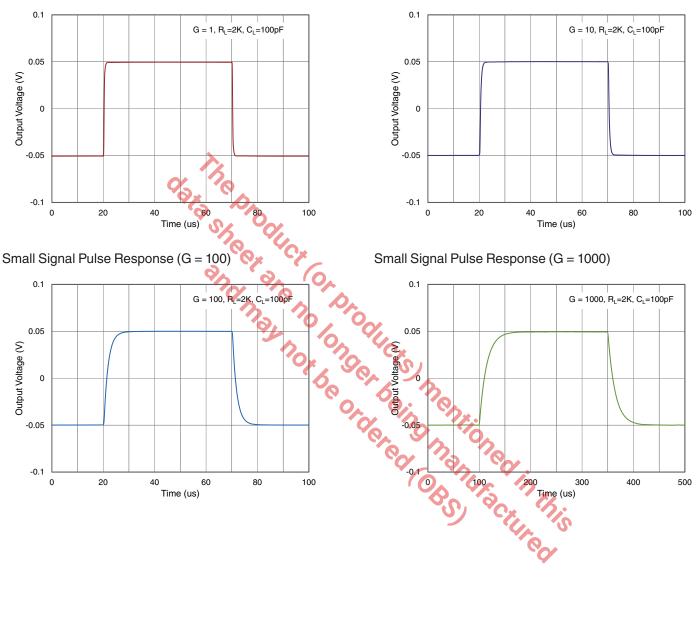
350

400

450

 $T_A = 25^{\circ}C$ ,  $V_S = \pm 15V$ ,  $R_L = 2k\Omega$  to GND; unless otherwise noted.

### Small Signal Pulse Response (G = 1)



Small Signal Pulse Response (G = 10)

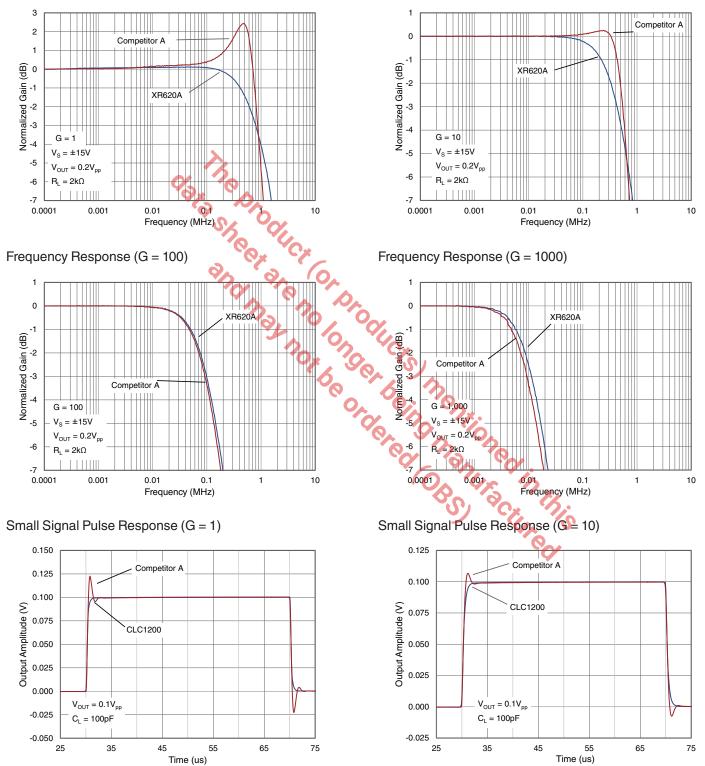
© 2013-2015 Exar Corporation

# **Typical Competitive Comparison Plots**

 $T_A = 25^{\circ}C$ ,  $V_S = \pm 15V$ ,  $R_L = 2k\Omega$ , Exar evaluation board; unless otherwise noted.



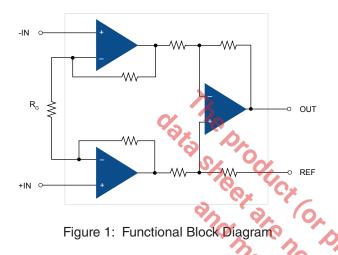
Frequency Response (G = 10)



# **Application Information**

#### **Basic Information**

The XR620A is a monolithic instrumentation amplifier based on the classic three op amp solution, refer to the Functional Block Diagram shown in Figure 1. The XR620A produces a single-ended output referred to the REF pin potential.



The internal resistors are trimmed which allows the gain to accurately adjusted with one external resistor  $R_G$ .

$$G = \frac{49.4k}{R_G} + 1; \quad R_G = \frac{49.4k}{G - 1}$$

 $R_G$  also determines the transconductance of the preamp stage. As  $R_G$  is reduced for larger gains, the transconductance increases to that of the input transistors. Producing the following advantages:

- Open-loop gain increases as the gain is increased, reducing gain related errors
- Gain-bandwidth increases as the gain is increased, optimizing frequency response
- Reduced input voltage noise which is determined by the collector current and base resistance of the input devices

#### **Gain Selection**

The impedance between pins 1 and 8,  $R_G$ , sets the gain of the XR620A. Table 1 shows the required standard table values of  $R_G$  for various calculated gains. For G = 1,  $R_G = \infty$ .

1% R <sub>G</sub> (Ω)	Caclulated Gain	0.1% R <sub>G</sub> (Ω)	Calculated Gain
49.9k	1.990	49.3k	2.002
12.4k	4.984	12.4k	4.984
5.49k	9.998	5.49k	9.998
2.61k	19.93	2.61k	19.93
1.00k	50.40	1.01k	49.91
499	100.0	499	100.0
249	199.4	249	199.4
100	495.0	98.8	501.0
49.9	991.0	49.3	1,003.0

#### Table 1: Recommended R<sub>G</sub> Values

Follow these guidelines for improved performance:

- To maintain gain accuracy, use 0.1% to 1% resistors
- $\hfill\blacksquare$  To minimize gain error, avoid high parasitic resistance in series with  $R_G$
- To minimize gain drift, use low TC resistors (<10ppm/°C)</li>

## **Common Mode Rejection**

The XR620A offers high CMRR. To achieve optimal CMRR performance:

Connect the reference terminal (pin 5) to a low impedance source

Minimize capacitive and resistive differences between the inputs

In many applications, shielded cables are used to minimize noise. Properly drive the shield for best CMRR performance over frequency. Figures 1 and 2 show active data guards that are configured to improve AC common-mode rejections. the capacitances of input cable shields are "bootstrapped" to minimize the capacitance mismatch between the inputs.

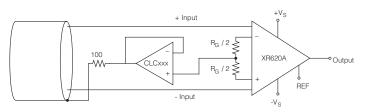


Figure 2: Common-mode Shield Driver

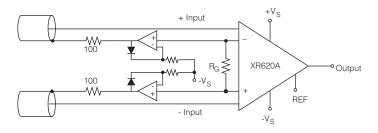


Figure 3: Differential Shield Driver

#### **Pressure Measurement Applications**

The XR620A is especially suitable for higher resistance pressure sensors powered at lower voltages where small size and low power become more significant.

Figure 3 shows a  $3k\Omega$  pressure transducer bridge powered from 5V. In such a circuit, the bridge consumes only 1.7mA. Adding the XR620A and a buffered voltage divider allows the signal to be conditioned for only 3.8mA of total supply current. Small size and low cost make the XR620A especially attractive for voltage output pressure transducers. Since it delivers low noise and drift, it will also serve applications such as diagnostic noninvasive blood pressure measurement.

#### **Medical ECG**

The XR620A is perfect for ECG monitors because of its low current noise. A typical application is shown in Figure 4. The XR620A's low power, low supply voltage requirements, and space-saving 8-lead SOIC package offerings make it an excellent choice for battery-powered data recorders.

Furthermore, the low bias currents and low current noise, coupled with the low voltage noise of the XR620A, improve the dynamic range for better performance.

The value of capacitor C1 is chosen to maintain stability of the right leg drive loop. Proper safeguards, such as isolation, must be added to this circuit to protect the patient from possible harm.

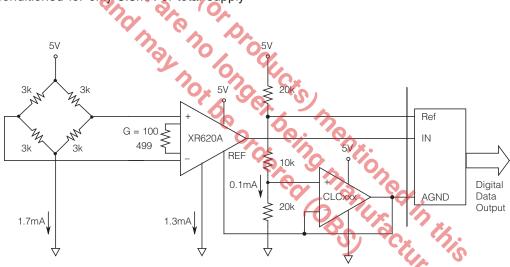


Figure 4: Pressure Monitoring Circuits Operating on a Single 5V Supply

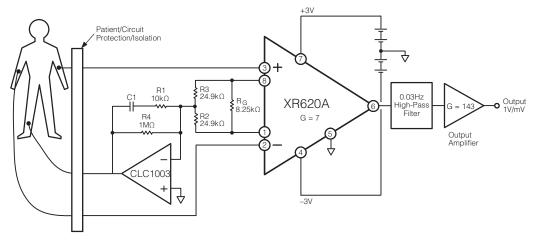


Figure 5: Typical Circuit for ECG Monitor Applications

#### Grounding

The output voltage of the XR620A is developed with respect to the potential on the reference terminal (pin 8). Simply tie the REF pin to the appropriate "local ground" to resolve many grounding problems.

To isolate low level analog signals from a noisy digital environment, many data acquisition components have separate analog and digital ground pins. Use separate ground lines (analog and digital) to minimize current flow from sensitive areas to system ground. These ground returns must be tied together at some point, usually best at the ADC.

#### Layout Considerations



General layout and supply bypassing play major roles in high frequency performance. Exar has evaluation boards to use as a guide for high frequency layout and as an aid in device testing and characterization. Follow the steps below as a basis for high frequency layout

- Include 6.8µF and 0.1µF ceramic capacitors for power supply decoupling
- Place the 6.8µF capacitor within 0.75 inches of the power pin
- Place the 0.1µF capacitor within 0.1 inches of the power pin
- Remove the ground plane under and around the part, especially near the input and output pins to reduce parasitic capacitance
- Minimize all trace lengths to reduce series inductances

Refer to the evaluation board layouts below for more information.

### **Evaluation Board Information**

The following evaluation boards are available to aid in the testing and layout of these devices:

Evaluation Board #	Products
CEB024	XR620A in SOIC-8

#### **Evaluation Board Schematics**

Evaluation board schematics and layouts are shown in Figures 6-8. These evaluation boards are built for dualsupply operation. Follow these steps to use the board in a single-supply application:

- 1. Short -V<sub>S</sub> to ground.
- 2. Use C3 and C4, if the -V\_S pin of the amplifier is not directly connected to the ground plane.

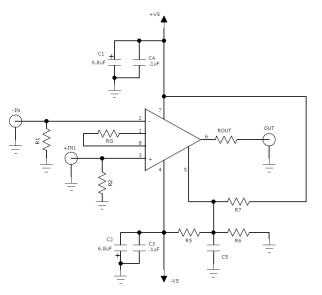
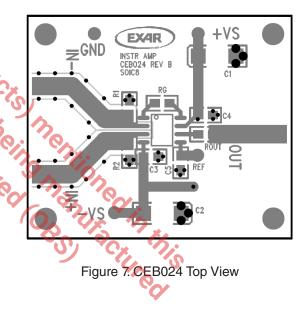


Figure 6. CEB024 Schematic



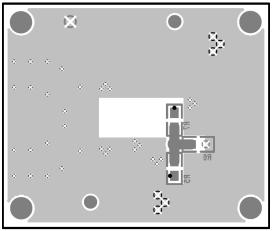
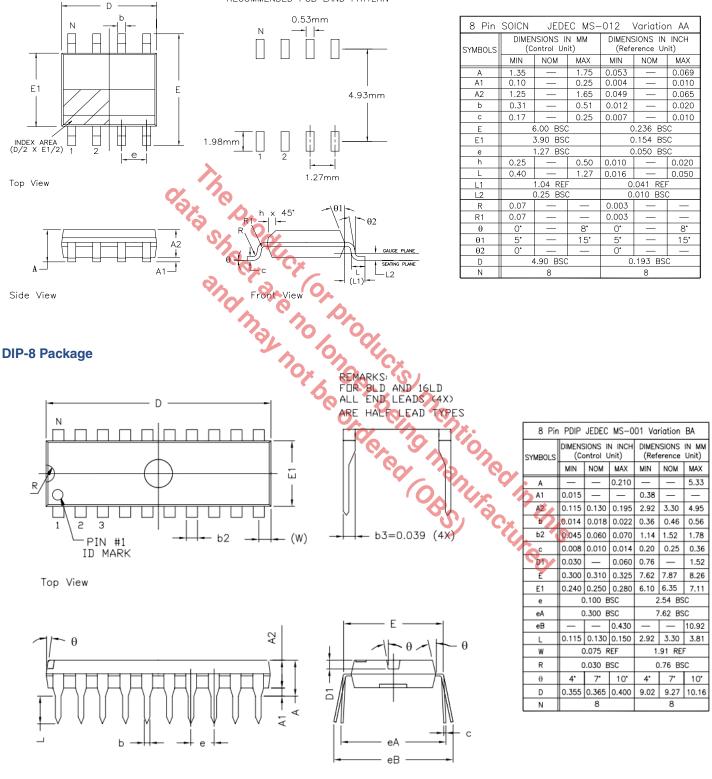


Figure 8. CEB024 Bottom View

# **Mechanical Dimensions**

#### **SOIC-8 Package**

RECOMMENDED PCB LAND PATTERN



Side View

Front View

# **Ordering Information**

Part Number	Package	Green	Operating Temperature Range	Packaging
XR620AISO8X	SOIC-8	Yes	-40°C to +85°C	Tape & Reel
XR620AISO8MTR	SOIC-8	Yes	-40°C to +85°C	Mini Tape & Reel
XR620AISO8EVB	Evaluation Board	N/A	N/A	N/A
XR620AIDP8	DIP-8	Yes	-40°C to +85°C	Rail

Moisture sensitivity level for all parts is MSL-1. Mini Tape and Reel contains 250 pieces.

# **Revision History**

Revision	Date	Description
1B (ECN 1513-05)	March 2015	Reformat into Exar data sheet template. Updated PODs and thermal resistance numbers. Updated ordering information table to include MTR and EVB part numbers. Updated evaluation board top and bottom views to Rev b. Added schematic used for evaluation boards.
	2	Con Cr
		d p p p p
		ordering information table to include MTR and EVB part numbers. Updated evaluation board top and botom views to Rev b. Added schematic used for evaluation boards.
		or berging
		Ord Cing Ontio
		red maned :
		- CUP S
For Further Assistance		pport@exar.com
Email: CustomerSupport@exar.		

#### Exar Corporation Headquarters and Sales Offices

 48760 Kato Road
 Tel.: +1 (510) 668-7000

 Fremont, CA 94538 - USA
 Fax: +1 (510) 668-7001

#### NOTICE

EXAR Corporation reserves the right to make changes to the products contained in this publication in order to improve design, performance or reliability. EXAR Corporation assumes no responsibility for the use of any circuits described herein, conveys no license under any patent or other right, and makes no representation that the circuits are free of patent infringement. Charts and schedules contained here in are only for illustration purposes and may vary depending upon a user's specific application. While the information in this publication has been carefully checked; no responsibility, however, is assumed for inaccuracies.

EXAR Corporation does not recommend the use of any of its products in life support applications where the failure or malfunction of the product can reasonably be expected to cause failure of the life support system or to significantly affect its safety or effectiveness. Products are not authorized for use in such applications unless EXAR Corporation receives, in writing, assurances to its satisfaction that: (a) the risk of injury or damage has been minimized; (b) the user assumes all such risks; (c) potential liability of EXAR Corporation is adequately protected under the circumstances.

Reproduction, in part or whole, without the prior written consent of EXAR Corporation is prohibited.